

Synthesis and deformation mechanics of gradient nanostructured materials

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Abstract The emerging gradient nanostructured metals and alloys containing spatially graded structural components with large variations in length scale and/or mechanical properties exhibit unprecedented mechanical performance. This perspective delineates the basic structural features of gradient nanostructures, *i.e.* structural components and spatial gradients, as well as related synthesis methods, excellent tensile properties, and novel deformation mechanisms. The challenges and prospect for the development of gradient nanostructured materials in the future are also addressed.

Keywords Gradient nanostructure, Spatial gradient, Synthesis, Mechanical property, Work hardening, Deformation mechanism

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Achieving both strength and ductility at the same time is a long-lasting pursuit for metallic materials. Inspired by biological materials in nature with spatial gradients in local chemical composition or constituents and/or structural characteristics at the nanoscale, which generally exhibit a good combination of strength and toughening, spatial gradients have been introduced into metallic materials [1]. The broad tunability of the gradient nanostructure (GNS) opens new frontiers for the development of high-performance metals and alloys for more challenging applications. In recent years, the emerging GNS metals and alloys have received the growing attention of the materials community due to their unprecedented mechanical properties, such as a combination of superior strength and ductility and enhanced fatigue resistance compared to non-gradient counterparts [2–8].

Large amounts of experimental, computational, and theoretical studies have been devoted to investigate the design, fabrication, and mechanical performance of several gradient nanostructured metals and alloys [1–4, 9–11]. Despite the rapid advance made in the past decade, fundamental understanding of the mechanical behavior of GNS metallic materials is still in its infancy. In this perspective, we reviewed the basic features of gradient nanostructures, tensile properties, and novel deformation mechanisms. In addition, insights into the challenges and opportunity in the field of GNS metals and alloys are provided.

As a typical hierarchical nanostructure, the two salient features of the gradient nanostructure are 1) structural components and 2) continuous/discontinuous but ordered spatial distributions. Basically, the structural components may include the grain size, twin or lamellar thickness, dislocation

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density or pattern size, and dual-gradient structure of both grain size and twin thickness that are spatially varied, as shown in [Figures 1a–1d](#). The extensively studied chemical gradients including graded distributions in the phase, solid–solution concentration and chemical components in biological materials [\[1\]](#) will be not discussed in this paper. Besides the types of basic structural components, their spatial distribution is another key characteristic of GNS, which differs from the homogeneous or random distribution of structural components. Accordingly, the gradient structure composed of the above-mentioned structural components can be either concentrated only in the sample surface ([Figure 1e](#)) or filled in the whole sample level with monotonous ([Figure 1f](#)), symmetric ([Figure 1g](#)), or multi-periodic spatial variations ([Figure 1h](#)). Here, structural gradient, s , a quantitative factor to describe the spatial distribution degree of the GNS, is defined as the increment in hardness per unit thickness along the gradient direction in [Figure 1f](#). The multiple structural components and distribution characteristics offer a spectrum of feasible pathways toward tailor-designing mechanical properties of GNS materials.

More importantly, we would like to emphasize that only when the characteristic size of any structural component refines as small as possible (that is so-called ‘go to nano’) and the multi-scaled hierarchies’ (or properties) discrepancy of sample-level gradient structure becomes as large as possible (*i.e.* the length scales span six to seven orders of magnitude), the advantages of gradient nanostructures as well as the novel deformation mechanisms can be more significantly achieved or activated.

The typical processing techniques used to synthesize GNS metals contain top-down methods *via* plastic deformation and bottom-up approaches *via* chemical (such as electro-deposition) or physical techniques. Surface mechanical treatment procedures, including surface mechanical attrition treatment, surface mechanical grinding treatment, shot peening, *etc.* [\[12\]](#), have been well developed to introduce surface gradient nanograined (GNG) structure ([Figures 1a](#) and [1e](#)). However, the GNG layers introduced by these surface manufacturing approaches are universally located on the sample surfaces with a limited total volume fraction of 20–25%, wherein high-density dislocations prevail.

Electrodeposition technique is known for controllably synthesizing GNS samples with a gradient volume fraction of 100%, and low initial dislocation density [\[13\]](#). For instance, pure Ni samples possessing a GNG structure with a monotonic change in the grain size up to three orders of magnitude were

prepared by electrodeposition, where the degree of grain size gradient can be accurately tuned [\[14\]](#). Gradient nanotwinned (GNT) Cu samples [\[10\]](#) were also fabricated by direct-current electrodeposition with a controllable patterning of homogeneous nanotwinned (NT) components from monotonous, symmetric periodic to multi-periodic spatial variations, as shown in [Figures 1f–1h](#). These GNT samples exhibit a dual-gradient distribution in both grain size and twin thickness ([Figure 1d](#)). Although it exhibits precise controllability, this chemical approach can only be used to introduce GNS structures in a few pure metals with low deposition rates. Other universal and efficient innovative synthesis methods are in urgent need for preparing varied GNS; more importantly, they should be widely feasible for more engineering alloys.

Recently, a simple, yet efficient cyclic-torsion (CT) treatment without any surface tooling was successfully developed to introduce novel sample-level gradient nanoscale stable dislocation structures (GDS) with low-angle boundary misorientations ([Figures 1c](#) and [1g](#)) with a length scale spanning six magnitudes from millimeter to nano scale in engineering materials, such as 304 stainless steel [\[15\]](#) and high entropy alloy (HEA) [\[11\]](#). In particular, the initial grain structure, including grain size and morphology, is unchanged from the surface to the core, which is fundamentally distinct from the GNG structure with a severely refined grain size. Owing to its controllably tuned variable torsion parameters, such as torsion angle amplitude and torsion number, this new promising paradigm for tailoring properties by engineering stable gradient-dislocation patterns at the nanoscale can be potentially applicable to any metallic materials dominated by dislocation mechanisms.

Both structural component and spatial distributions play vital roles in determining the mechanical properties of the gradient nanostructure. The tensile stress–strain curves of interstitial-free (IF) steel with a surface GNG layer is shown in [Figure 2a](#), as an example [\[9\]](#). Due to the presence of surface GNG layer (with a limited volume fraction of 25%), the yield strength of GNG/CG IF steel doubles, whereas its ductility is slightly reduced, compared to that of the coarse-grained (CG) counterparts ([Figures 2a–2b](#)). A similar phenomenon was universally observed in other GNG metals and alloys, such as Cu, Ni, and 316 steels [\[12\]](#). However, owing to the limited GNG volume fraction and structural gradient, the strength of these samples with an GNG/CG architecture roughly follows the rule-of-mixture according to that of the GNG surface layers and CG substrate core. Meanwhile, the work

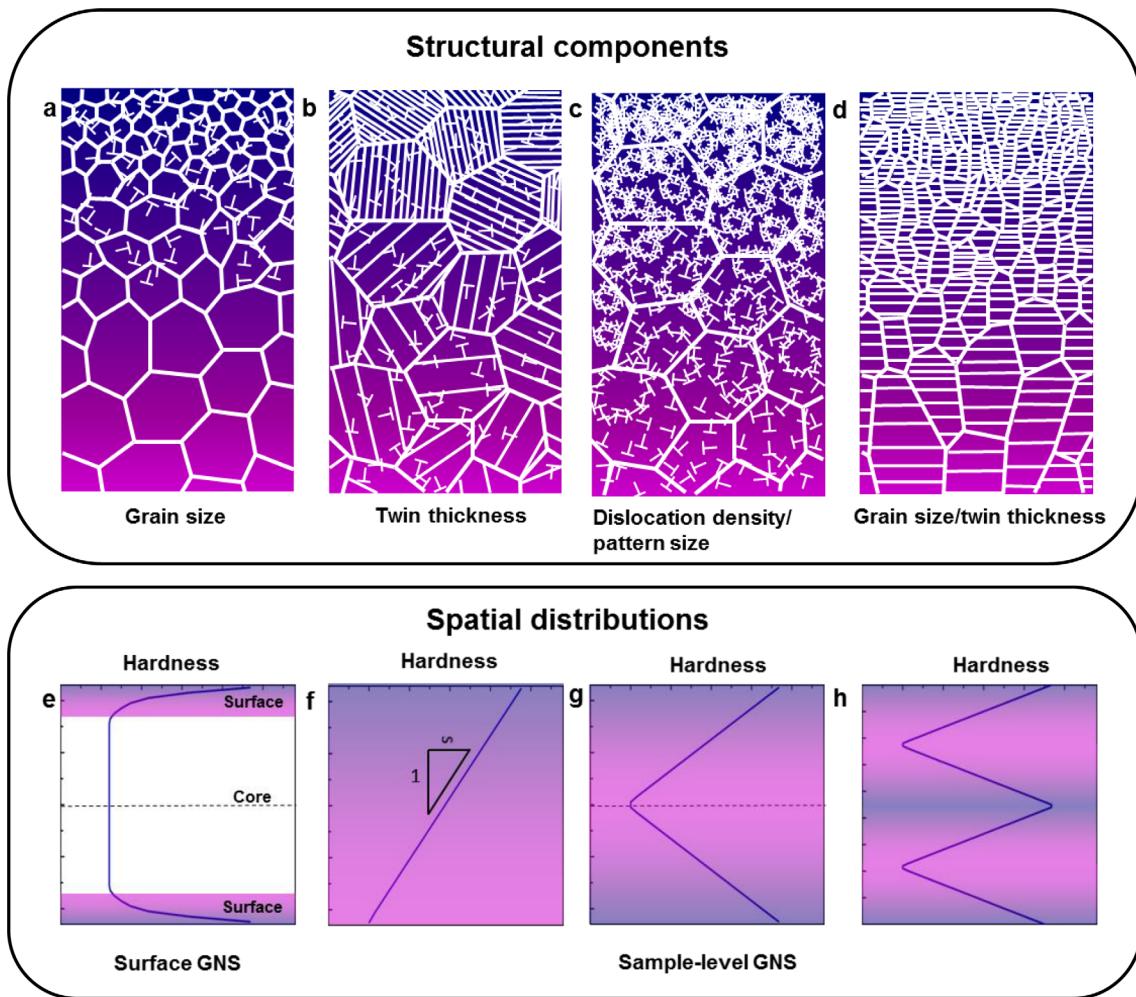


Figure 1. Structural components and spatial distributions in gradient nanostructured (GNS) materials. Structural components contain grains size (a), deformation twin thickness (b), dislocation density or pattern size (c), and both the grain size and twin thickness (d). Spatial distributions include the GNS either in the sample surface (e) or in the sample level with monotonous (f), symmetric (g), or multi-periodic spatial variation (h).

hardening and tensile plasticity of GNG/CG samples strongly rely on their CG substrate (Figure 2b). A mechanically driven grain boundary migration process with grain coarsening or shear band and resultant softening were proposed to dominate the plastic deformation of GNG structures [12].

The presence of nano-scale twin components remarkably elevates the mechanical properties of GNT Cu samples. Simultaneous enhancement in strength and work hardening rate can be achieved by solely increasing the structural gradient, that even exceeds the strongest component, yet accompanied by a slight reduction in the uniform elongation, indicative of extra strengthening and work hardening (Figures 2c-2d). Such an unprecedented strength-ductility combination primarily stems from the sample-level stable NT component with large structural gradients,

that cannot be achieved by any other structure. Moreover, gradient order also affects the tensile properties, *i.e.* a higher strength can be achieved in GNT Cu with normal gradient order (hard surfaces and soft core), compared to those with reverse gradient order (soft surfaces and hard core) [16].

When sample-level gradient dislocation patterns (Figure 1c) are introduced in a single fcc phase Al_{0.1}CoCrFeNi HEA by CT treatment [11], it exhibits a three-fold higher yield strength while maintaining steady work hardening, and comparable tensile plasticity, compared to its CG counterparts. Such an exceptional synergy of strength and ductility has not been possibly achieved in homogeneous or heterogeneous structures and most existing metals and alloys with gradient nanograins or nanotwins.

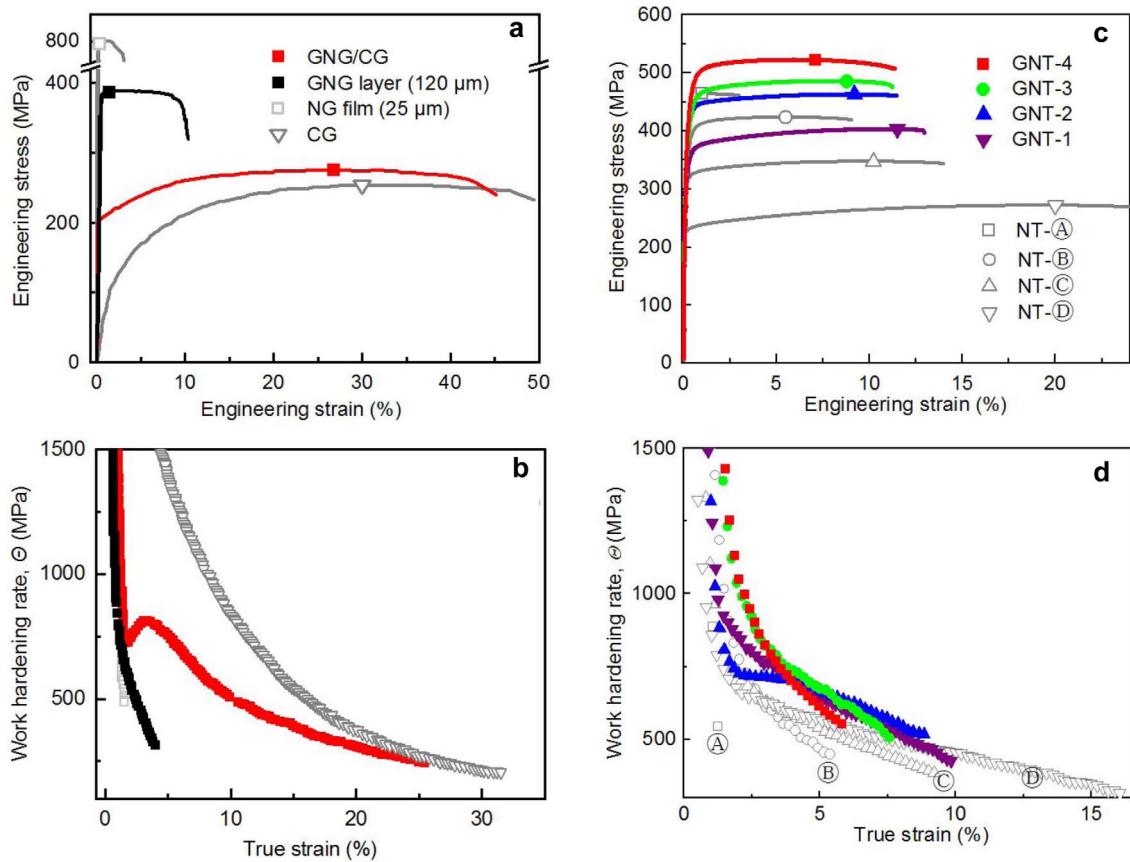


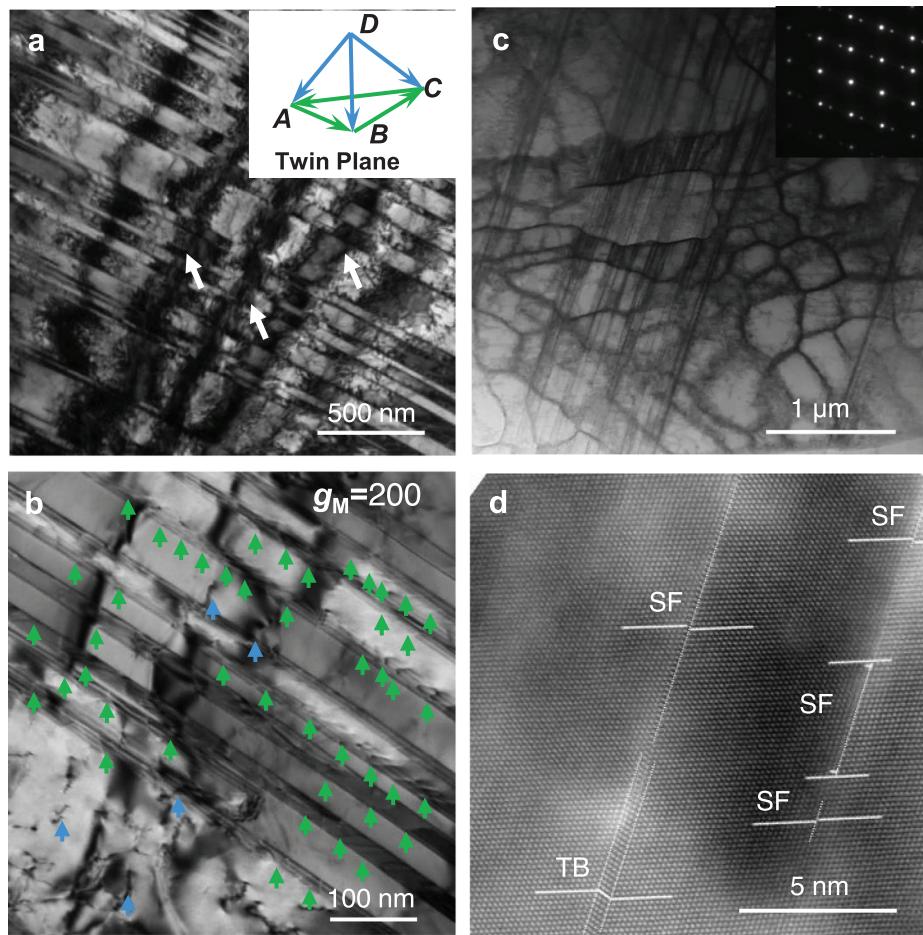
Figure 2. Superior mechanical properties of GNS materials. Tensile engineering stress–strain relations (a, c) and variation in work hardening rate with respect to true strain (b, d) of GNG IF steel (a, b) and GNT Cu (c, d) samples, compared with their homogeneous components. [Figures (a) and (b) were adapted with permission from ref. [9], PNAS. Figures (c) and (d) were adapted with permission from ref. [10], AAAS.]

During the deformation of GNS materials, the structural gradient induces plastic deformation incompatibility, *i.e.* a remarkably ordered, progressive deformation transformation from elasticity to plasticity due to yield strength discrepancy among different structural components. The resultant deformation incompatibility is generally accommodated through the generation of geometry necessary dislocations (GNDs) based on the theoretical models [17–20], which further leads to a built-in gradient in both plastic strain and stress, as demonstrated by experiments [10], theories, and modeling [4, 21, 22]. Such inhomogeneous deformation on the scale of the structural gradient fundamentally differs from the case in conventional metallic materials without gradient. In particular, some novel dislocation activities, interface-related behavior, and interactions between GNDs and interfaces have been observed.

For example, a brand new dislocation pattern with bundles of concentrated dislocations (BCDs) is

formed and uniformly distributed in the grains of GNT Cu at a small tensile strain (Figure 3a) [10]. These BCDs consist of both model I and II dislocations from different slip systems, illustrated by Thompson tetrahedron and marked by green and blue arrows, respectively, in Figure 3b. By contrast, only Mode II (green) dislocations are detected in the homogeneous NT component under the same loading condition. Coincidentally, a novel Shockley partial dislocation associated with stacking fault-induced plasticity (SFIP)-dominated strengthening mechanism, rather than the traditional full dislocations, is reported in the deformed GDS HEA [11]. After an initial tensile strain as small as 3%, highly dense micrometer-length Stacking Fault (SF) bundles in Figure 3c, composed of sub-10-nanometer SFs and twins (Figure 3d), are progressively activated to mediate the plastic deformation of GDS HEA.

Without a doubt, either the presence of BCDs with ultrahigh density of dislocation in GNT samples



Bundle of concentrated dislocations

Stacking fault-induced plasticity

Figure 3. Structural gradient-induced novel deformation mechanisms. Bundles of concentrated dislocations (BCDs) in GNT Cu at 1% strain, indicated by the white arrows (a), which are identified by two-beam diffraction using vectors of $g_M = 200$ (b). Highly dense micrometer-length SF bundles in the GDS HEA at 3% strain (c), which are composed of numerous sub-10-nanometer SFs and tiny twin boundaries (TBs) (d). The inset in (c) is the corresponding selected area electron diffraction patterns containing parallel streaks from SFs. [Figures (a) and (b) were adapted with permission from ref. [10], AAAS. Figures (a) and (b) were adapted with permission from ref. [11], AAAS.]

or high density of tiny SFs in GDS samples are products of the deformation of the gradient nanostructure and also products of GND-assisted deformation. These novel dislocation patterns in the GNS microstructure can act as strong obstacles to further dislocation slips and the sustainable sources for dislocation nucleation and storage. These distinctive structural component-dependent deformation mechanisms are crucial to maintain structural stability across multiple scales and suppress softening. Macroscopically, the sample-level orderly and progressive plastic strain in GNS samples effectively relaxes the local stress concentration between adjacent components of different length sizes and suppresses strain localization, enabling different

structural components of the gradient nanostructure sample to plastic deform coherently, even at a higher overall stress level. As a result, extra strengthening and extra work hardening or an unprecedented better combination of strength and ductility can be achieved in both GNT and GDS materials. This effect will become more pronounced when the structure gradient becomes larger.

Despite the considerable progress made in processing and mechanics of GNS metals and alloys, there are still several open issues and challenges ripe for future experimental, analytical, and modeling studies. Further innovation in processing techniques is desired for precisely tailoring gradient nanostructures with multiple structural components and

spatial gradients. The development of more cost-effective, yet efficient techniques with scale-up capability for GNS engineering materials is necessary for promoting their industrial production and application.

Since the current design and optimization of gradient nanostructures remain largely empirical, it becomes urgent to develop quantitative theoretical and computational modeling frameworks to designing and optimizing multiscale structural parameters to achieve targeted mechanical properties. Multiscale modeling, atomistic simulation, and theoretical studies should be strengthened to reveal the novel deformation mechanism and address the role of structural gradient played on the novel mechanical responses. More multiscale advanced microstructural characterizations, including three-dimensional high-resolution transmission electron microscopy, in-situ synchrotron X-ray diffraction, and neutron diffraction characterizations, are expected and to be combined to explore the complicated structural and inhomogeneous stress/strain evolutions spanning different length scales.

Revealing the intrinsic mechanical properties, especially the service performance including fatigue, fracture, creep, corrosion, and wear, of various gradient nanostructures are still intriguing unexplored issues. Also, decoupling the multiple microstructural parameters, such as structural component, length scale, spatial distribution, structural gradient, and the volume fraction, on the mechanical behaviors of GNS metals and alloys is essential for further performance optimization; however, these related in-depth research works remain scarce. Finally, quantifying correlations among hierarchical gradient nanostructures, deformation mechanism, and damage behavior are essential for advancing the potential engineering applications of GNS materials.

Conflicts of Interest

The authors declare no conflict of interest.

Data Availability Statement

All data generated or analyzed during this study are included in this published article.

Author Contributions

L.L initiated and supervised the project. Q.P and L.L contributed to the discussions and wrote the manuscript.

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References

- [1] Suresh S. Graded materials for resistance to contact deformation and damage. *Science* 2001; **292**: 2447–51.
- [2] Fang TH, Li WL and Tao NR *et al.* Revealing extraordinary intrinsic tensile plasticity in gradient nano-grained copper. *Science* 2011; **331**: 1587–90.
- [3] Wei Y, Li Y and Zhu L *et al.* Evading the strength–ductility trade-off dilemma in steel through gradient hierarchical nanotwins. *Nat Commun* 2014; **5**: 1–8.
- [4] Li XY, Lu L and Li JG *et al.* Mechanical properties and deformation mechanisms of gradient nanostructured metals and alloys. *Nat Rev Mater* 2020; **5**: 706–23.
- [5] Roland T, Retraint D and Lu K *et al.* Fatigue life improvement through surface nanostructuring of stainless steel by means of surface mechanical attrition treatment. *Scr Mater* 2006; **54**: 1949–54.
- [6] Pan QS and Lu L. Improved fatigue resistance of gradient nanograined metallic materials: Suppress strain localization and damage accumulation. *Scr Mater* 2020; **187**: 301–6.
- [7] Lu L, Pan QS and Hattar K *et al.* Fatigue and fracture of nanostructured metals and alloys. *MRS Bull* 2021; **46**: 258–64.
- [8] Kou H, Lu J and Li Y. High-strength and high-ductility nanostructured and amorphous metallic materials. *Adv Mater* 2014; **26**: 5518–24.
- [9] Wu XL, Jiang P and Chen L *et al.* Extraordinary strain hardening by gradient structure. *Proc Natl Acad Sci USA* 2014; **111**: 7197–201.
- [10] Cheng Z, Zhou H and Lu Q *et al.* Extra strengthening and work hardening in gradient nanotwinned metals. *Science* 2018; **362**: 559–68.
- [11] Pan QS, Zhang LX and Feng R *et al.* Gradient cell-structured high-entropy alloy with exceptional strength and ductility. *Science* 2021; **374**: 984–9.
- [12] Lu K. Stabilizing nanostructures in metals using grain and twin boundary architectures. *Nat Rev Mater* 2016; **1**: 16019.
- [13] Lu L, Shen YF and Chen XH *et al.* Ultrahigh strength and high electrical conductivity in copper. *Science* 2004; **304**: 422–6.
- [14] Lin Y, Pan J and Zhou HF *et al.* Mechanical properties and optimal grain size distribution profile of gradient grained nickel. *Acta Mater* 2018; **153**: 279–89.

- [15] Pan QS, Guo S and Cui F *et al.* Superior strength and ductility of 304 austenitic stainless steel with gradient dislocations. *Nanomaterials* 2021; **11**: 2613, 1–9.
- [16] Cheng Z and Lu L. The effect of gradient order on mechanical behaviors of gradient nanotwinned Cu. *Scripta Mater* 2019; **164**: 130–4.
- [17] Ashby MF. The deformation of plastically non-homogeneous materials. *Philos Mag* 1970; **21**: 399–424.
- [18] Fleck NA, Muller GM and Ashby MF *et al.* Strain gradient plasticity: Theory and experiment. *Acta Metall Mater* 1994; **42**: 475–87.
- [19] Nix WD and Gao H. Indentation size effects in crystalline materials: a law for strain gradient plasticity. *J Mech Phys Solids* 1998; **46**: 411–25.
- [20] Gao HJ, Huang YG and Nix WD *et al.* Mechanism based strain gradient plasticity I Theory. *J Mech Phys Solids* 1999; **47**: 1239–63.
- [21] Zeng Z, Li X and Xu D *et al.* Gradient plasticity in gradient nano-grained metals. *Extreme Mech Lett* 2016; **8**: 213–9.
- [22] Zhang Y, Cheng Z and Lu L *et al.* Strain gradient plasticity in gradient structured metals. *J Mech Phys Solids* 2020; **140**: 103946.

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